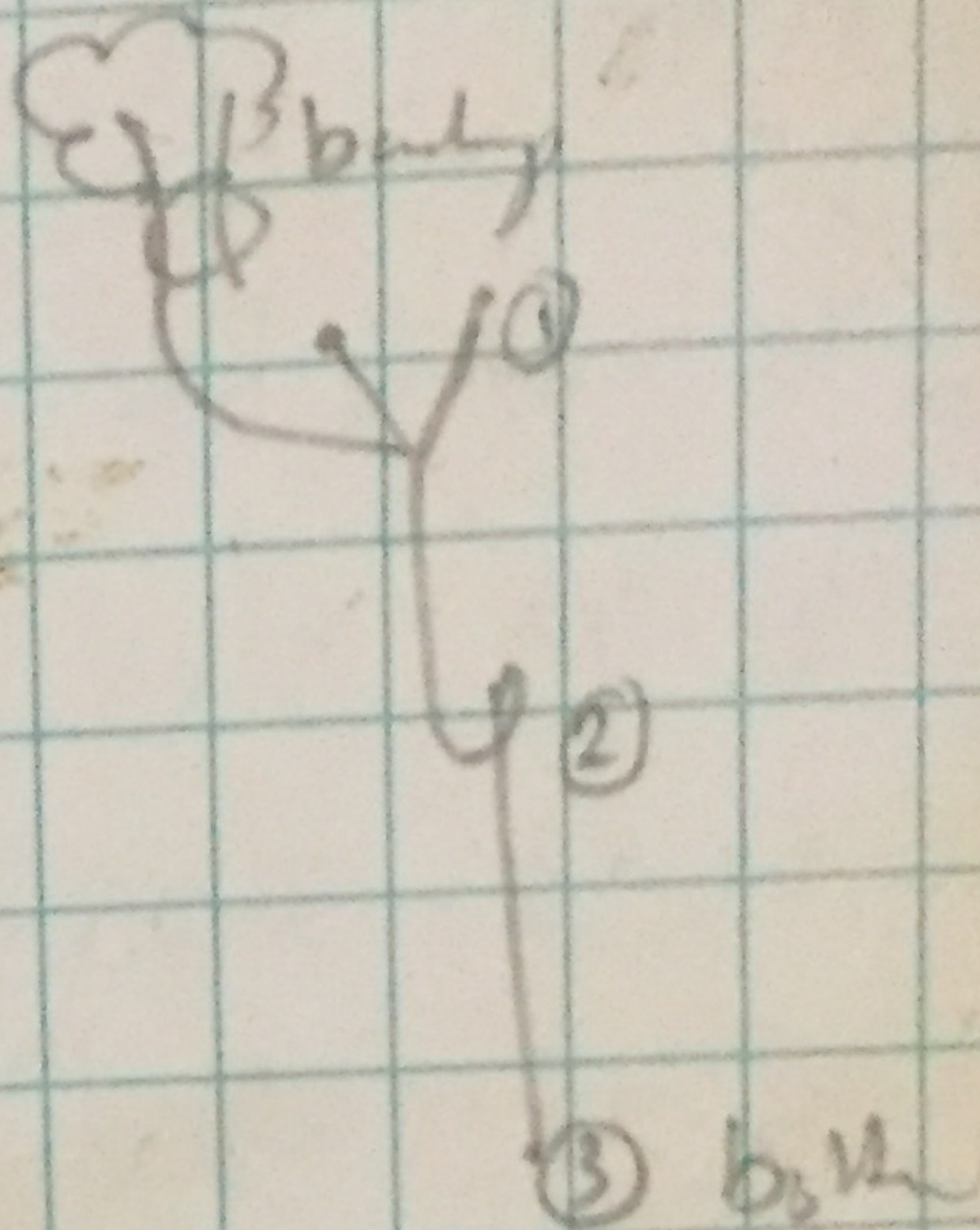
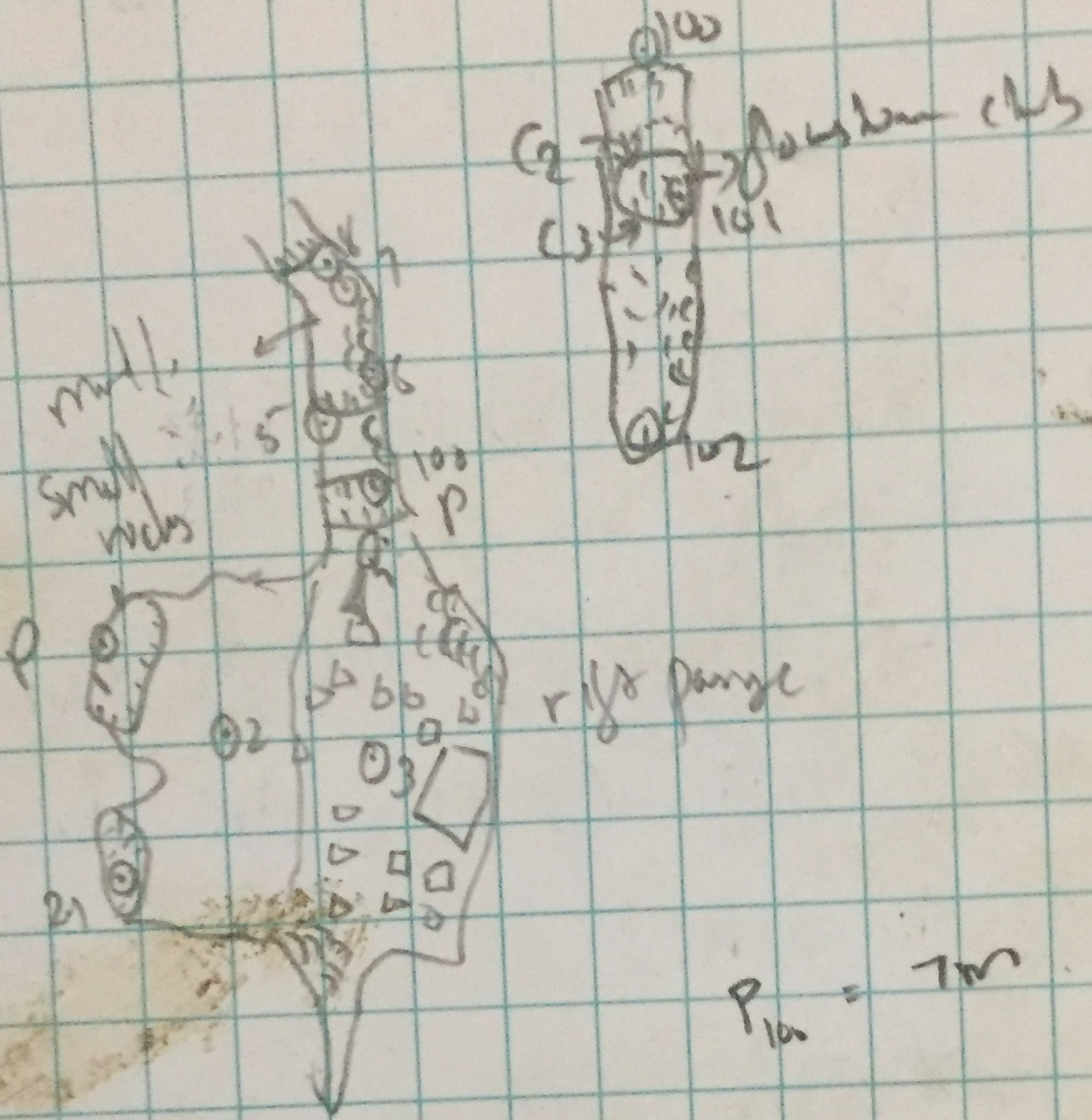
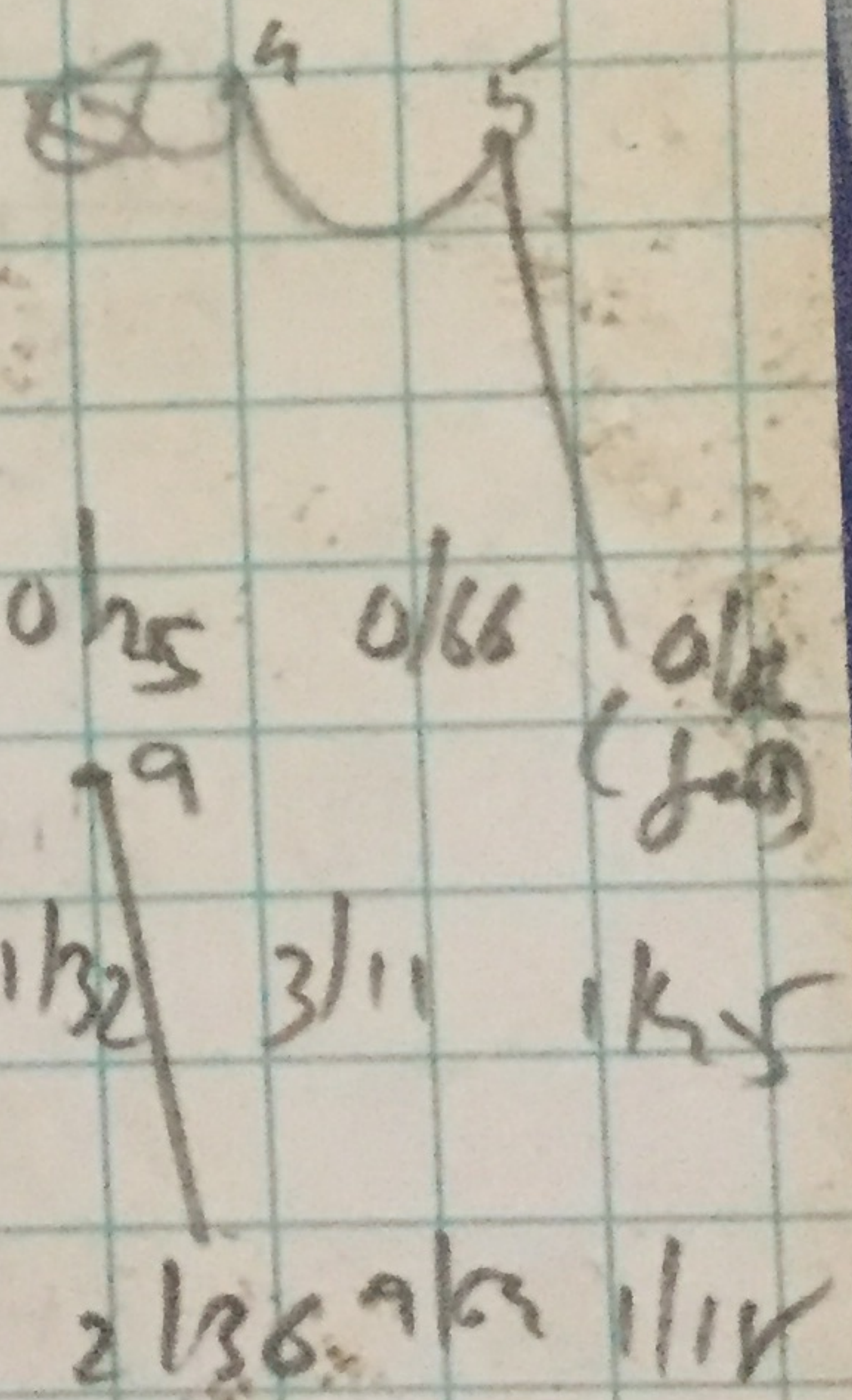


F	T	D	C	I	L	R	U	D
1 1	2	12/81	098/0	-00/4	⊙	60	054/00	23/10
2	2.1 seal entr	11/41	180/2	65/15				
2	3	10/22	076/7	-86/6	⊙	3/90	3/01 11/98	11/30
3	3.1	6/49	181/2	21/1				
3	4 (dent)	3/52	340/7	-14/1	⊙	2/54	1/76	9/41 1/04
4	5.1	7/67	33/68	-76/2	⊙	0/0	1/52	11/82 1/08 (sit)
4	8	4/71	358/4	-37/8				4/47 1/62
5	6	1/80 1/80	082/6	07/1	⊙	0/0	0/6	6/34 12/92 1/02 (not in butter)
6	7	12/72	205/1	-79/1				
7	8	1/83	244/3	-01/4	⊙	0/81	0/10	7/02 11/37
8	9	1/33	213/9	-05/4	⊙	0/30	0/53	4/72 1/63
9	10	6/99	288/6	-82/0	⊙	0/59	0/0	6/17 1/8 6/99
10	11	10/27	216/7	-89/1	⊙	1/48	do	7/61 13/03
11	12	11/60	071/7	-80/7	⊙	2/80	1/31	9/23 11/60
12	13	7/57	126/4	35/6	⊙	2/52	8/07	6/11 1/11

N ↑



$P_{100} = 7m$



4-100	4/28	178/1	04/2					
bb-101	5/43	22/5	-57.4	⊙ 0/3	0/5	0/66	0/6	(f)
101-102	10/90	22/8	5/5	⊙ 101	0/0	1/32	3/11	1/5
				⊙ 102	0/8	2/36	9/69	1/14

C2

F	T	D	C	$\frac{C_2}{\geq 1}$	L	R	U	D		
100	99	5/08	12/14	67/13	(100)	0/0	0/63	5/10	0/68	
99	98	1/57	0/12	2/11	(99)	0/28	0/55	0/0	0/94	
98	inlet	6/100	18/16	32/20	(98)	0/0	1/71 3/63	4/27	0/54	
98	97	3/33	14/6	23/2						
97	96	3/03	03/4	49/2	(97)	3/26	0/21	8/47	0/53	
96	95	2/34	115/6	13/7	(96)	2/13	1/35	3/19	0/88 (fed)	
95	?	5/16	352/9	-02/4					3/88 (5/11)	
95	94	2/79 4/38 2/80	105/5 104/7	6/6 6 2/5	(95)	0/0	0/4	3/26	1/58	
94	93	2/41	113/6	30/2	(94)	0/20	0/06	0/64	0/85	
93	(92)	2/13	206/7	19/9	(93)	0/0	0/73	0/82	1/68	
92	91	3/22	203/1	-04/5	(92)	1/4 8/20	0/61	0/0	1/65	
92	C2	2/78	13/18	25/6						
91	-100 211	6/60	200/1	-01/4	(91)	0/65	0/0	2/43	1/62	
91	90	3/42	235/10	-64/8						
90	89 Cohme2	4/44	158/5	35/1	(89)			1/86	1/13	0/94
90	88	2/4	31/2	-8/9	(90)	0/4	0/17 1/72	4/72	2/82	

17
211
3
2
19

